

THEORETICAL STUDY OF TURBULENT SALINE DIFFUSION
IN A CONDUIT IN CONTINUOUS SERVICE

Roger Lièvre

GPO PRICE \$ _____

CFSTI PRICE(S) \$ _____

Hard copy (HC) 1.00Microfiche (MF) .50

ff 653 July 85

FACILITY FORM 502

N67 10754

(ACCESSION NUMBER)

5

(PAGES)

(NASA CR OR TMX OR AD NUMBER)

(THRU)

(CODE)

(CATEGORY)

Translation of "Étude théorique de diffusion saline
turbulente en conduite en régime permanent."
Comptes Rendus des Séances de l'Académie des Sciences,
Vol. 244, pp. 1611-1614, 1957.

NOTICE

BECAUSE OF COPYRIGHT RESTRICTION THIS TRANSLATION HAS NOT BEEN PUBLISHED.
THIS COPY IS FOR INTERNAL USE OF NASA PERSONNEL AND ANY REFERENCE TO THIS
PAPER MUST BE TO THE ORIGINAL FRENCH SOURCE.

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
WASHINGTON
AUGUST 1964

THEORETICAL STUDY OF TURBULENT SALINE DIFFUSION
IN A CONDUIT IN CONTINUOUS SERVICE¹

/1

Roger Lièvre

ABSTRACT

The distribution of concentration in a point-type injection is obtained by solving the diffusion equation, after which the effect of hypothetical calculations on the solutions arrived at is examined.

In a previous paper, we achieved solutions of the diffusion equation. Supposing now that $c(z, \theta, 0)$ is the concentration at $\xi = 0$, the concentration on the abscissa ξ will be given by the equation

$$c(z, \theta, \xi) = \sum_{m=0}^{\infty} (b_{mp} \cos m\theta + c_{mp} \sin m\theta) \sum_{p=0}^{\infty} f_{mp}(z) e^{-\beta_{mp}\xi} \quad (9)$$

the coefficients b_{mp} and c_{mp} being calculated according to the classical methods applicable to orthogonal functions.

It is possible, for example, to start with the injection section and to consider the brine jet to be the equivalent of a semi-point discharge.

It should be noted that the discharge of salt is usually accomplished by a jet that causes a different turbulent diffusion from that existing in a conduit, and a higher one in any case. This procedure underestimates, then, mixture by diffusion.

We shall calculate in this way the concentration resulting from a point discharge at the coordinates $z = z_0$ and $\theta = 0$.

The following are the first useful terms of the development for numerical values of $k = 0.4$ and $n = 21$ in order of increasing damping:

¹Presented at the meeting, 11 March 1957.

$$z(1-z)f'' + (2-3z)f' + s \frac{u(z)}{U} f = 0. \quad (14)$$

or in our case

$$z(1-z)f'' + (2-3z)f' + \sigma(1-z^p)f = 0, \quad \sigma = s \frac{p+2}{p}. \quad (15)$$

The coefficients of the development of finite f for $z = 0$

$$f(z) = \sum_{n=0}^{\infty} a_n z^n \quad (16)$$

establish the recurrence equation

$$a_{n+1} = \frac{[n(n+2) - \sigma] a_n + \sigma \cdot a_{n-p}}{(n+1)(n+2)}. \quad (17)$$

Generally speaking, the series (16) does not converge for $z = 1$, except for the characteristic values of σ . These characteristic values can be obtained by the use of the continuity equation:

$$\int_0^1 f(z, \sigma) z(1-z^p) dz = 0. \quad (18)$$

To establish this property, we multiply the terms of (15) by z and integrate from 0 to 1 as follows: /3

$$[f' z^2(1-z)]_0^1 + \int_0^1 f(z, \sigma) z(1-z^p) dz = 0. \quad (19)$$

f is finite at point $z = 0$, but it has generally a logarithmic point at $z = 1$, the derivative f' being, therefore, of the form $a/(1-z)$, and the term between parentheses not being zero. For the characteristic values of σ , f remains finite, the term between parentheses is zero, and equation (18) is satisfactorily established. The integration, term by term, of f according to (18) gives the series

$$F(\sigma) = \sum_{n=0}^{\infty} a_n \frac{p}{(n+2)(n+p+2)}. \quad (20)$$

The convergence is gradual. We have calculated the first root, $\sigma = 4.166$, to 17 places, for $p = 6$. The corresponding value of s is 3.1245 instead of $s = 3$ in the case of a uniform distribution of velocities.

Thus the assumption that there is a uniform distribution of velocities leads to an acceptable approximation.

Translated for the National Aeronautics and Space Administration by
John F. Holman and Co. Inc.